# General Methodology for Determining As-Constructed and Subsequntly Improved Condition (ACSIC)



RCWD Board Workshop February 12, 2024



#### Purpose of Workshops

- Workshop #1: Provide an understanding of how ACSIC's are determined state-wide
- Workshop #2: Provide an understanding of how this methodology was utilized in RCWD and specifically on ACD 10-22-32

#### These workshops are NOT:

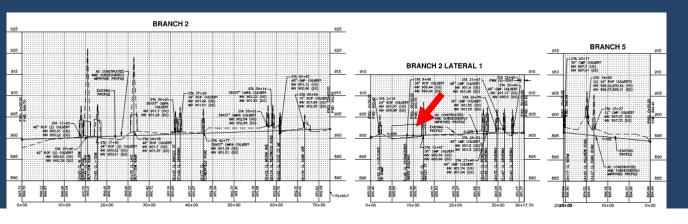
- An attempt by consultant/staff to prove prior conclusions
- A reopening of the drainage proceedings

(Note: Board may reopen proceedings when new information, not previously considered, brings into question the adopted ACSIC)



## What is the ACSIC and Why is It Important?

- As-Constructed (as-built) condition
- Includes alignment, profile (grade), x-section, and right-of-way
- Basis for maximum repair (M.S. 103E.701 Subd. 1)
- Includes improvement/modification under M.S. 103E and predecessors
- Does not generally include modifications outside of M.S. 103E (but some exceptions)
- Is not the as-designed condition (though as-designed condition can inform)
- Is not a decision/policy
- ACSIC is a factual condition (repeatable & scientific basis)

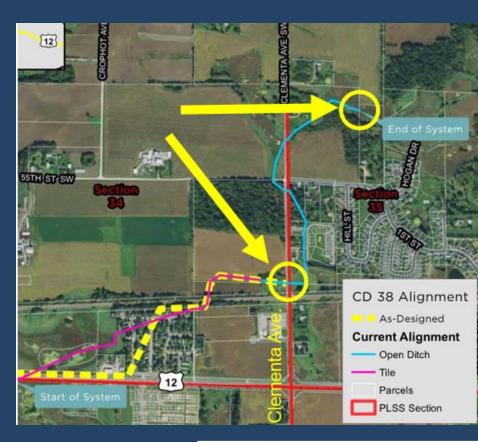




- 1. Determine as-built (ACSIC) and As-Designed Alignment
  - Basis for As-Designed/ACSIC profile

#### **Relevant Documents**

- Historic maps
- Establishment documents
- Aerial photography
- LiDAR topography





# 2. Field SurveyRelevant Information

- Channel bottom (200' spacing)
- Cross-sections (1,000' spacing)
- Soil borings/soil probes (1,000' spacing)
- Culverts and roadways
- 3. Map survey data in CAD







4. Review historic documents and identify relevant information

#### <u>Relevant Documents – Establishment & Improvement</u>

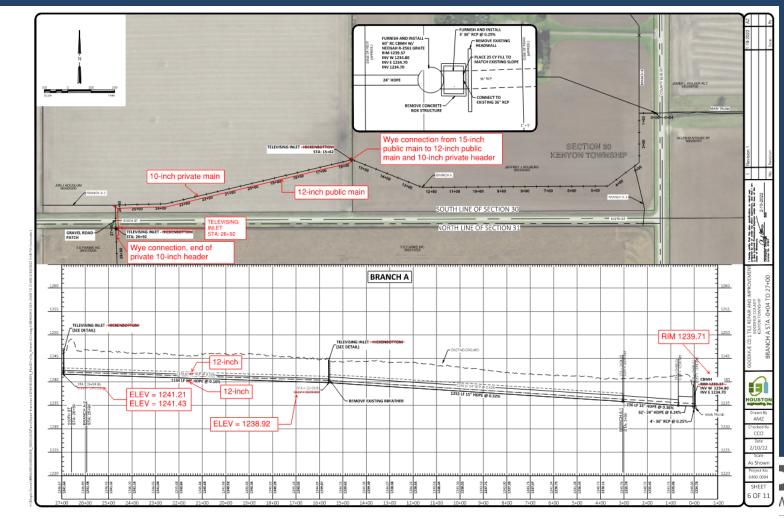
- As-built drawings (Rare!)
- As-designed profile drawings
- As-designed cut depths

#### Relevant Documents – Other 103E Actions

- Repairs
- Inspection Reports
- Realignment/Impoundment/Abandonment

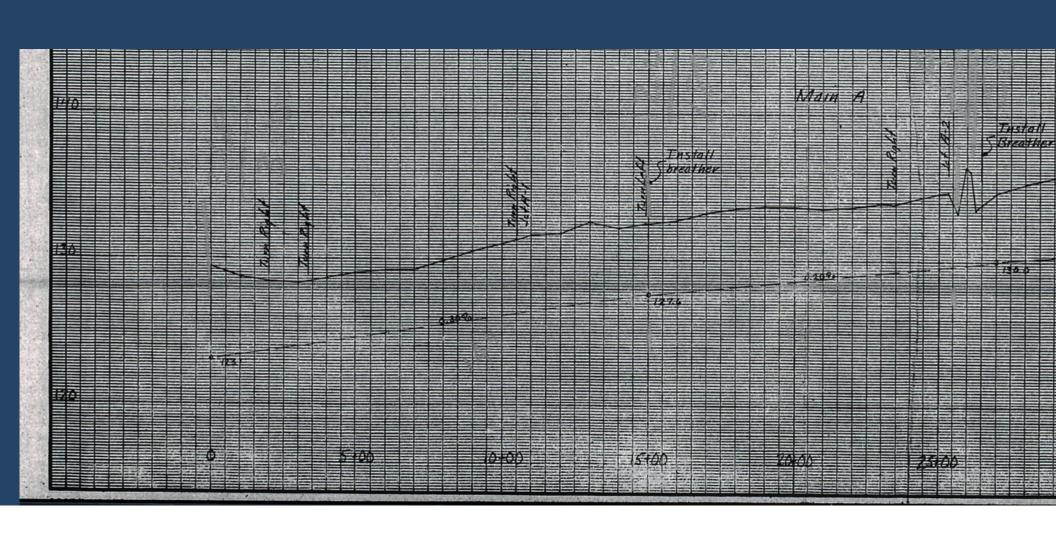


# Example Relevant Documents – As-Builts





# Example Relevant Documents – Historic Profile



## **Example Relevant Documents – Cut Depths**

#### EXHIBIT 2 OF ENGINEER'S REPORT IN DITCH PROCEEDINGS.

No. 2562 Engineer's Report in Ditch Proceedings.

Showing Estimated Depth of Cut, Width, No. of Cubic Yards Removed and Cost of Same, in Main Ditch No. 24

|     |                      | (1)          | (2)                    | (3)                 | (4)                              | (5)                            | (6)  |             |      | (7)                                    |
|-----|----------------------|--------------|------------------------|---------------------|----------------------------------|--------------------------------|--|-------------|------|--|
| 9   | SECTION              | DEPTH OF CUT | MIDTH OF CUT AT BOTTOM | WIDTH OF CUT AT TOP | NO. OF CUBIC YARDS TO BE REMOVED | Estimated Cost Per Cubic Yards | Character of Other Expenses, Including Preliminary Exp<br>And Expense of Inspecting Work Until Completed<br>With Total Per Section | oenses<br>l |      | Total<br>Estimated Cost<br>per Section |
|     |                      |              |                        |                     |                                  | \$ CTS.                        |  | \$ (        | CTS. | \$ CTS.                                |
|     | Between Stake No. O  | 3.20 /1      | 1.5 ft                 | 7. 90 ft.           |                                  | 015                            |  |             |      |  |
|     | and Stake No.        | 1.92"        | "                      | 5. 34.              | 38.50                            | 4                              | think it is a second   |             |      | 577                                    |
|     | Between Stake No. 2  | 1.37"        | 11                     | 4.24,               | 19.26                            | 4                              |  |             |      | 2 89                                   |
|     | and Stake No. 3      | 1.32,        |                        | 4.14 "              | 14.26                            | I+                             |  |             |      | 214                                    |
|     | Between Stake No. 4  | 1.07,        | h                      | 3.64,               | 11:85                            | "                              |  |             |      | 178                                    |
|     | and Stake No. 5      | 1. 22,       | 4                      | 3.94.               | 11.29                            |                                |  |             |      | 169                                    |
| No. | Between Stake No.    | 1.37         | 4                      | 4.24.               | 13.34                            | . 4                            |  |             |      | 200                                    |
| 43  | and Stake No. 7      | 1.60         | n.                     | 4.80                | 16.84                            | 9                              |  |             |      | 203                                    |
| 100 | Between Stake No.    | 1.601        | 9:                     | 4.70.               | 18.73                            | 7                              |  |             |      | 281                                    |
|     | and Stake No. 9      | 1.55         | tr.                    | 4.60 "              | 17.86                            | 9                              |  |             |      | 268                                    |
|     | Between Stake No. // | 1.500        | "                      | 4.50,               | 17.18                            | w                              |  |             |      | 258                                    |
|     | and Stake No.        | 2.201        | *                      | 5.90 "              | 22.96                            | 70                             |  |             |      | 3 44                                   |
|     | Between Stake No /2  | 2.15.        |                        | 5.80 ,              | 29.73                            | 7                              |  |             |      | 446                                    |
|     | and Stake No. 3      | 2.001        | 4                      | 5,50                | 27.38                            | 4 -                            |  |             |      | 411                                    |
| 4   | Between Stake No. 14 | 2,60,        |                        | 6.70                | 32.37                            | ,                              | a bridge or culvert  | 40          | 00   | 4 85                                   |
| 5   | and Stake No.        | 2.444        | 9                      | 6.38 .              | 37.52                            | 9                              | V.   |             |      | 563                                    |
| 4   | Between Stake No. /6 | 2.24.        | 4                      | 5.98 1              | 33, 31                           | W.                             |  |             |      | 499                                    |
| 惠   | and Stake No. 17     | 2.441        | 9                      | 6.38                | 3 3, 31                          | 4                              |  |             |      | 499                                    |
| NA. | Between Stake No. /8 | 3.44,        | 31                     | 8.38                | 48.36                            | "                              |  |             |      | 725                                    |
|     | and Stake No.        |              | Water Control          |                     | 444.05                           |                                |  | 40          | 00   | 6 6 60                                 |



Total Estimated Cost of Whole Work, \$

For Sale by Miller-Davis Printing Co., Mfg. Stationers, Minnespolls.

### **Example Relevant Documents – Other**

**RESOLUTION 2006-10** 

RICE CREEK WATERSHED DISTRICT BOARD OF MANAGERS

FINDINGS and ORDER DIRECTING PARTIAL ABANDONMENT
OF ANOKA COUNTY DITCH 55
WITHIN the CITY OF CENTERVILLE

Manager <u>Lerou.</u> V offered the following Resolution and moved its adoption, seconded by Manager <u>Hocke</u>:

#### **FINDINGS**

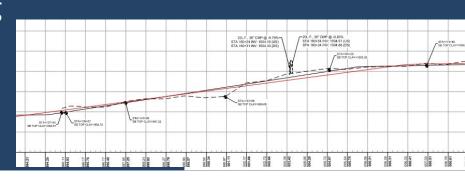
 The Rice Creek Watershed District is the drainage authority for the Anoka County Ditch 55 (ACD 55) system.

2. On May 2, 2006, in conjunction with work under RCWD Permit 06–052, the Anoka County Transportation Department ("Petitioner") filed with the RCWD a petition to abandon that portion of ACD 55 from the northern boundary of CSAH 14 (Main Street) south a distance of 760 feet, more or less, to the northern terminus of the portion of ACD 55 to be realigned by the City of Centerville pursuant to RCWD

| OM | (3)<br>WIDTH OF CUT<br>AT TOP | NO. OF CURE<br>TO BE BE | MOVED   | (5)<br>Estimated Cost<br>Per Cuber Yard<br>5 GTS | Charister at Octor B | (6)<br>Expenses, Including Pr<br>Inspecting Works Us<br>with Potal per Section | eliminary Expenses<br>All Completed | Estimated Out | 100 TO |        |             |            |      |             |             |           |          |                |             |                       |        |
|----|-------------------------------|-------------------------|---------|--|----------------------|--|-------------------------------------|---------------|--|--------|-------------|------------|------|-------------|-------------|-----------|----------|----------------|-------------|-----------------------|--------|
| ,  | 7.0                           | in old ;<br>Ditch       | Removed | /2   |                      |  |                                     | 328           |  |        |             |            |      |             |             |           |          |                |             |                       |        |
|    | 7.0                           | 12.6                    | 27.3    |  |                      |  |                                     | 5 34          | <u> </u>                                   |        |             |            |      |             |             | -         | -        |                |             |                       |        |
|    | 7.0                           | 14.8                    | 29.6    |  |                      |  |                                     | 355           | 1  | _ Tot  | WIDTH - 4   |            |      |             | WER<br>1100 |           |          |                |             |                       |        |
|    | 7.2                           | 19.6                    | 27.4    |  |                      |  |                                     | 329           | 1  | 100    | WILL THE ST | 1          |      | 3           | 2 2 2       | TOP OF RO | 10.10030 |                |             |                       |        |
|    | 2.0                           | 19.6                    | 24.8    |  |                      |  |                                     | 298           | 4  | - \    | 4×3·4       | / *        | 12   |             | /::\        |           |          |                |             |                       |        |
| 1  | 7.2-                          | 19.6                    | 24.8    |  |                      |  |                                     | 350           | 1  |        | PICAL SECT  | 1/0N<br>#5 |      |             | /\          | MY 887.86 |          |                |             |                       |        |
|    | 7.8                           | 20.4                    | 29.2    |  |                      |  |                                     | 350           | \$10                                       | E=0.0% |             |            | 100  | 886.93      |             | )         | 520      | PE =0.18%      |             |                       |        |
|    | 7.4                           | 19.6                    | 300     |  |                      |  |                                     | 340           | 4  |        |             | -00        |      |             | 90LF - 36"  | CARP 10   | -0¤      |                |             |                       | 15-100 |
| -  | 7.2                           | 19.6                    | 27.4    |  |                      |  |                                     | 298           | 1  |        |             |            |      |             |             |           |          | ::::\b         |             |                       |        |
|    | 7.0                           | 19.6                    | 24.8    |  |                      |  | 2                                   | 298           | 1  |        | <b>N</b>    |            | 5-4" |             |             |           |          | 30             |             |                       |        |
|    | 7.4                           | 19.6                    | 24.8    |  | 1                    |  |                                     | 2.98          |  | 70     | vical sec   | row        |      |             |             |           |          | 98             |             |                       |        |
| -1 | 7.8                           | 18.5                    | 28.5    |  |                      |  |                                     | 342           | 1  |        | 8.45 - 261  | 0          |      |             |             |           |          |                | -INK 890.   | 0AD 89633             |        |
| -  | 7.0                           | 18.5                    | 125     |  | 1                    |  |                                     | 3 42          | 52076                                      | 0.78%  |             |            |      |             |             | LOVE OF   | WY 890   | -              |             | SLOPE + D             | 07%    |
|    | 2.8                           | 14.8                    | 32.1    | 1 1  | 1                    |  | .                                   | 400           |  |        | 20          | 00:        |      |             |             | 2.5       | 00:      | 466.7          | 36"cM#      |                       | 30.00  |
| 1  | 7.4                           | 163                     |         |  |                      |  |                                     | 436           |  |        |             |            | 12   |             | W/ h-       | 2.27      |          |                |             |                       |        |
| (  | 7.8                           | /3.3                    | 1 444   |  | /                    |  |                                     | 472           |  |        |             |            | 20   | B-F-B"      | ON          |           |          | TOP OF DI      | M 89494     |                       | ▽      |
| -  | 7.0                           | 120                     | 550,    |  |                      |  | 11.079                              | 2866.00       | 1  | 1980   | SEC         | PF - 0.227 |      | 26-30 - 43- | 00          |           |          | - DITC# BUT    | Jun 3712    | :::SLOPE:             | 0.48%  |
|    |                               |                         |         |  |                      |  |                                     | 30.00         |  |        | 35          | -00        |      |             |             | 40        | 00       |                | 9           |                       | 48:00  |
|    |                               |                         |         |  |                      |  |                                     | 9534          |  |        |             |            |      |             |             |           |          |                | 99          |                       |        |
|    |                               |                         |         |  |                      |  | 1900                                | 8 4 70P       | or AMP 87                                  | 99     |             |            |      |             |             |           |          |                | - 22        |                       |        |
|    |                               |                         |         |  |                      |  |                                     |               |  |        |             | WATE       |      | FLEVATA     | 200 - 094.4 | 14        |          | - 2.0/ak.Mo/ : |             | ∆                     |        |
|    |                               |                         |         |  |                      |  | 1.890                               | 45100 MV 8928 | 30'RCP                                     | and a  | 50          | .00        | 540A | 0.07%       |             |           | 00       |                | ::: 27°CM   |                       | 60-00  |
|    |                               |                         |         |  |                      |  |                                     | SLOPE : 0.48  |  |        |             |            |      |             |             |           |          |                |             |                       |        |
|    |                               |                         |         |  |                      |  |                                     |               |  |        |             |            |      | CEK WATE    |             |           |          |                | HICKOK & AS | SOCIATES<br>ENGINEERS |        |

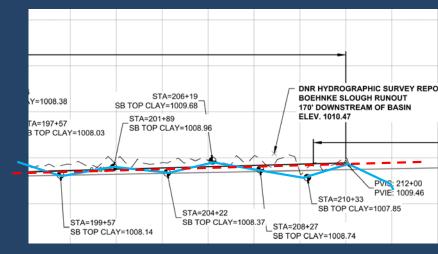
- 5. Compare boring elevations to historic profile\*
  - Datum Conversion: Difference between historic plan datum/benchmark (unknown) and sea level
    - Initial guess = average difference between boring and historic profile elevations
- 6. Plot adjusted as-designed profile using datum conversion

|        | Historic | Historic  | Probe     |            |
|--------|----------|-----------|-----------|------------|
| Branch | STA      | Elevation | Elevation | Difference |
| CD4    | 0+00     | N.A.      | N.A.      | N.A.       |
| CD4    | 5+00     | 96.8      | N.A.      | N.A.       |
| CD4    | 10+00    | 96.6      | 1151.22   | 1054.62    |
| CD4    | 15+00    | 96.4      | 1152.94   | 1056.55    |
| CD4    | 20+00    | 96.2      | 1153.26   | 1057.06    |
| CD4    | 25+00    | 96        | 1152.22   | 1056.23    |
| CD4    | 30+00    | 95.8      | 1151.35   | 1055.54    |
| CD4    | 35+00    | 95.6      | 1150.83   | 1055.22    |
| CD4    | 40+00    | 95.4      | 1149.96   | 1054.56    |
| CD4    | 45+00    | 95.2      | 1149.58   | 1054.37    |
| CD4    | 50+00    | 95        | 1148.71   | 1053.68    |



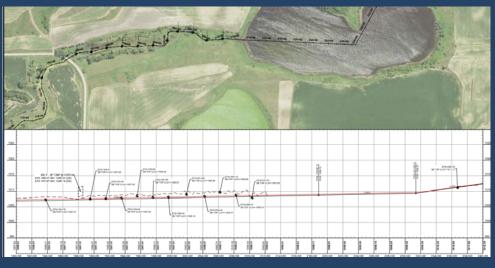
<sup>\*</sup>If one exists

- 7. Check for correlation between adjusted asdesign profile and soil borings
  - A. Good correlation throughout\*
    - Proceed to Step 8
  - B. Good correlation on portion
    - Recompute datum conversion on smaller segment
  - C. Locations of poor correlation (or no design profile)
    - Create a "trendline" (best fit) through borings
    - <u>Not</u> "dot-to-dot"....generalize



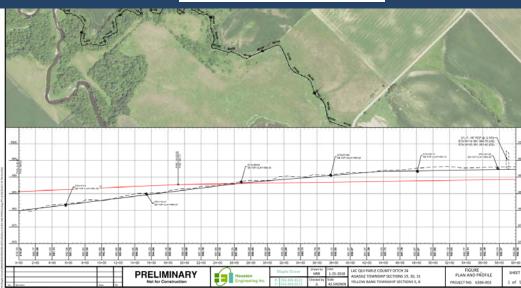


# Do the As-Designed Profile "Fit"?

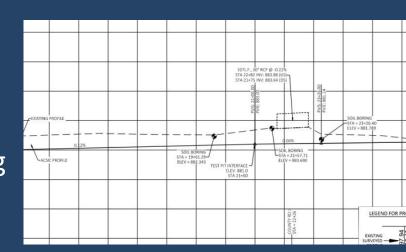


**Good Correlation** 

#### **Poor Correlation**



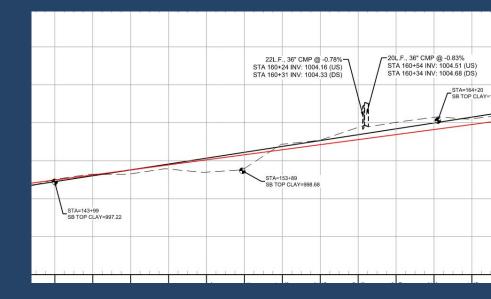
- 8. Consider other collected data
- 9. Identify "outliers" (borings substantially above/below profile and "breaks in logic" (e.g. negative slope, elevation not matching at branch intersections)
  - Can these be reconciled?
  - If not, obtain additional data:
    - Test pits
    - Additional borings
    - Revisiting documents





# Why a Single Boring/Probe/Test Pit May Not Be Reflective of ACSIC

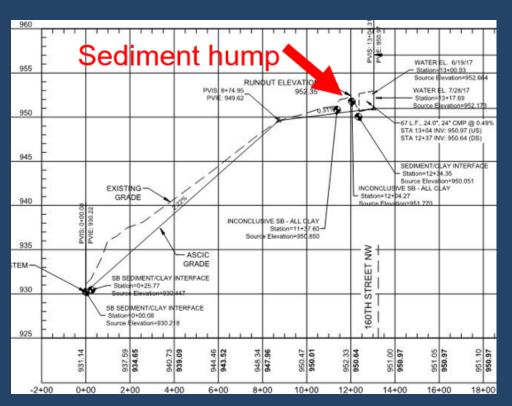
- Not in center of channel
- Bank sloughing
- Scour
- Over-excavation
- Settlement/subsidence
- Precision/accuracy
- ACSIC didn't reach "hardpan"

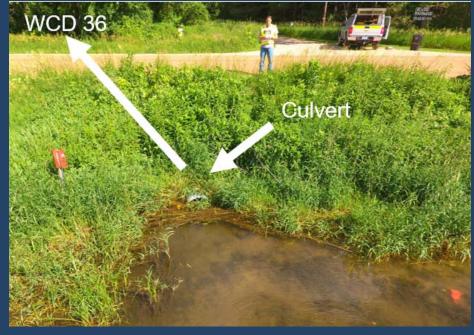




# **Example - Outlier**

#### Wright County Ditch 36 – channel sloughing

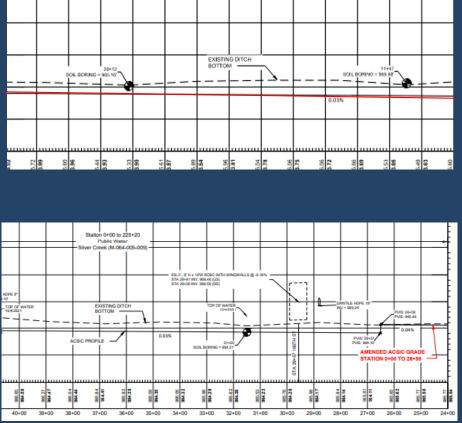


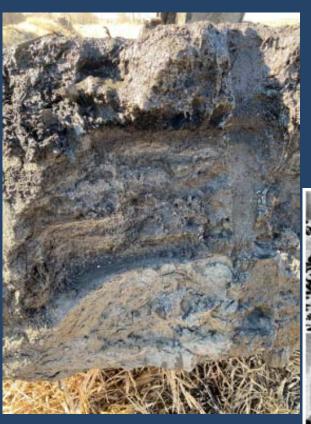


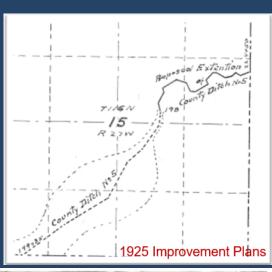


# Example – Break in Logic

#### McLeod County Ditch 5 – improvement

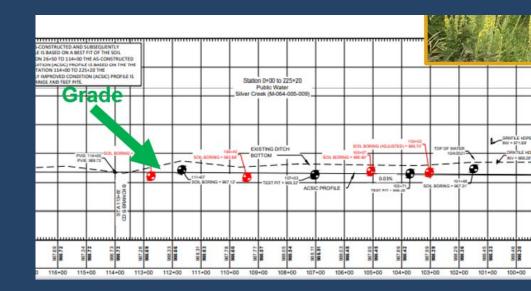








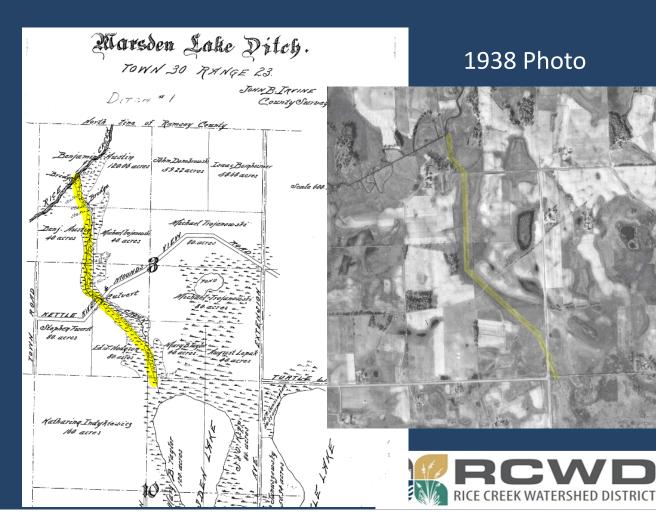
- 10. Internal (HEI) review\*
- 11. External review\*
  - Drainage authority staff
  - DNR
  - Public
  - Drainage authority board



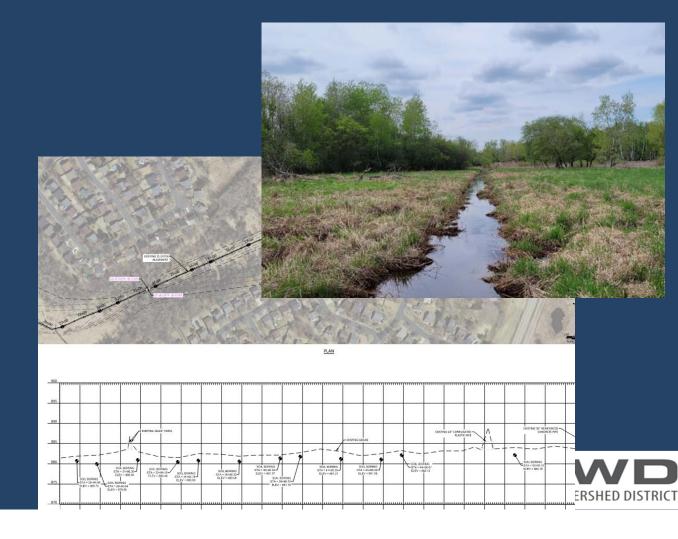
\*Any unresolved concerns require revisiting prior steps



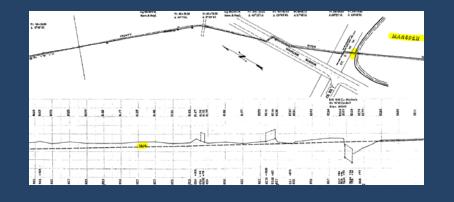
- 1. Alignment
- 2. Survey
- 3. Mapping
- 4. Historic Docs
- 5. Compare Elevations
- 6. Plot as-designed profile
- 7. Check Correlation
- 8. Consider other data
- 9. Identify Outliers
- 10. Internal review
- 11. External review

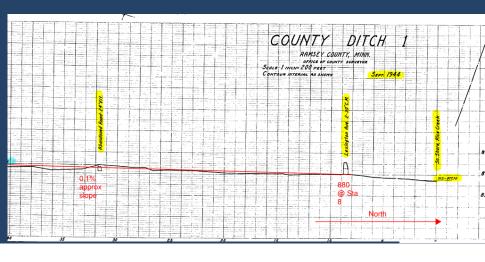


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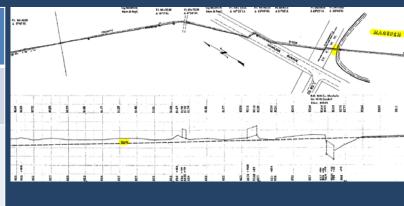
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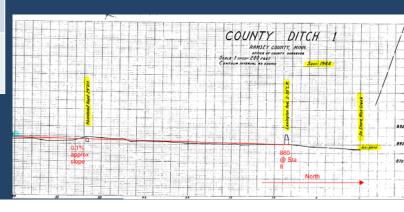




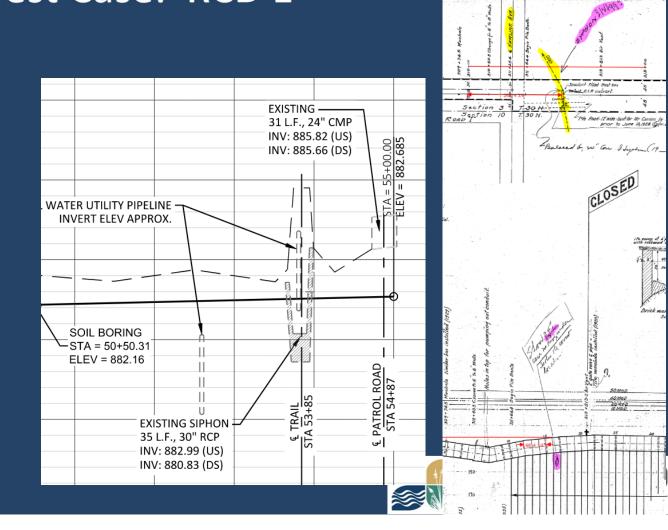
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| Source                       | Grade       |
|------------------------------|-------------|
| 1940 Repair                  | 0.1% (est). |
| 1985<br>Inspection<br>Report | 0.1%        |
| Mid-80's<br>repair           | 0.114%      |
| 2023 Borings                 | 0.116%      |





- 1. Alignment
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- 4. Historic Docs
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# RCWD Example – Critical Data

| System | Critical Data Components in ACSIC Determination |
|--------|---|
| ACD 31 | Test pits and as-designed profile               |
| ARJD 1 | Soil borings and as-designed profile            |
| RCD 2  | Ditch improvement profile and soil borings      |
| RCD 8  | Soil borings, test pits, and impoundment plan   |
| RCD 4  | Soil borings and culvert elevations             |

# Workshop #1 Takeaways

- Every system is different. Weighing of evidence varies by type and extent of available data.
- Process needs to be as objective and repeatable <u>as</u> <u>feasible</u>.
- Engineer must use multiple lines of evidence. There will be conflicting data. Cannot rely on a single point of data.
- <u>Evaluation Standard</u>: What is the profile with the greatest weight of evidence
- Judgement calls by the Engineer are required

